

A theoretical model of a Sr-90 nuclear battery

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In this paper a theoretical nuclear battery based upon a GaN Schottky diode is analyzed with a Sr-90 source. This theoretical battery was calculated to produce 17.52 nW from a 1 cm^2 1 mCi source. The fill factor of the theoretical device was calculated to be 0.5732 and the efficiency is 1.52%. The theoretical power of this battery shows an increase in power compared to the same device using a Ni-63 source of the same parameters. It is discussed that the use of Sr-90 as a radioisotope for a nuclear battery is not practical with current technology due to radiation damage and inability to create GaN semiconductors with a low dopant concentration and sufficiently large depletion regions.

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I. INTRODUCTION

The nuclear battery was a technology studied in the early 1950's and 1960's, its use was for applications that require a long battery life such as medical implants¹. In the 1970's the emergence of lithium batteries put a damper on the research of nuclear batteries due to the increased efficiency, and lower cost. Today there has been a re-emergence of the technology with better manufacturing techniques for semiconductors as well as radiation resistant materials.

The design of a nuclear battery is analogous to that of a solar cell. Incident radiation on the battery causes electron hole pairs in a material that diffuse into a depletion region where a built in electric field moves the charge carriers. The charge is collected in an anode and cathode on the device and current is produced. In solar cell operation the radiation is photons, in a nuclear battery the incident radiation is typically charged particles such as a β particle (electron) or a α particle (helium nucleus). These charged particles are emitted from a radioactive source and are used to create electron hole pairs in the semiconductor device. In the early development of the nuclear battery, alphavoltaics and betavoltaics were used with a silicon based P-N junction device. The resultant nuclear batteries were of low efficiency and the α particles caused damage to the silicon crystal structure and further reduced the efficiency of the devices².

The recent increase in research in nuclear batteries has been with betavoltaics in particular. Some common radioactive isotopes used in betavoltaic devices are Ni-63 with a half-life of 101.6 ± 1.97 years³ and H-3 (Tritium) with a half-life of 12.3 years⁴. These isotopes are ideal for a betavoltaic due to their long half-lives and that they are purely β emitters. A particular limitation of these isotopes is the low decay energy of the β particles, Ni-63 has a max decay energy of 66.98 KeV⁵ and H-3 has a max decay energy of 18.6 KeV⁶. The power output of a betavoltaic is proportional to the incident radiation energy, it is suggested that a higher energy β emitter is investigated such as Sr-90 to yield greater power.

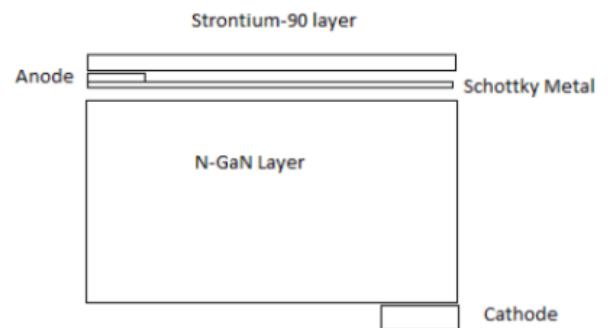


FIG. 1. Theoretical Schottky GaN based Betavoltaic

In this article a theoretical nuclear battery based upon a GaN, Schottky based Sr-90 betavoltaic is proposed. Strontium-90 is a beta emitter with a max β decay energy of 0.546 MeV⁷. It also has a half life of 28.8 years⁷. Strontium-90 is also purely a β emitter, which is favourable from a radiation hazard standpoint. The chosen betavoltaic design is based upon a Schottky barrier GaN based battery due to the high radiation resistance of metal (Schottky barrier) and GaN's large radiation resistance⁸.

II. EXPERIMENTAL PROCEDURE

The theoretical betavoltaic will use a thin layer of Schottky metal placed upon a N-GaN epilayer, with electrodes placed upon Schottky layer and N-GaN layer refer to Fig. 1. To determine the performance of the device, various parameters were calculated using MatLab.

A. β particle range in GaN

To determine the optimal depletion width of the GaN based Schottky betavoltaic the range of electrons in the

GaN must be determined. To determine the β range the Katz-Penfold range equation was used. The equation is as follows⁹

$$R_{max} = \frac{0.412}{\rho} E_{\beta}^{1.265-0.0954(E_{\beta})}; \quad (1)$$

$$0.01 \leq E_{\beta} \leq 2.5 \text{ MeV}$$

Where ρ is the density of the material (GaN) and E_{β} is the kinetic energy of the incident β particle. The range was calculated for a distribution of energies from $E_{\beta} = 0$ to $E_{\beta} = 0.546 \text{ MeV}$

The penetration depth was also calculated at the average energy beta decay \bar{E}_{β} 0.196 MeV. The depth was found to be $66 \mu\text{m}$, which can be taken as an approximate target for the depletion width. The entire spectra of β range is from 0-300 μm , to make a GaN semiconductor with a depletion region in the 100's of μm requires a very low charge carrier concentration that can not yet be manufactured.

Determining the depletion width will factor into determining the power characteristics of the betavoltaic and the efficiency. The depletion region width for a schottky barrier diode can be determined by¹⁰

$$W = \sqrt{\frac{2\epsilon_s \phi_i}{qN_D}} = \sqrt{\frac{2\epsilon_s(\phi_b - kT \ln(N_C/N_D))}{qN_D}} \quad (2)$$

Where

- ϵ_s dielectric constant of GaN
- ϕ_i build in potential
- N_D doping concentration
- N_C conduction band density of states of GaN
- ϕ_b Schottky barrier height
- k Boltzmanns constant
- T absolute temperature

Inspecting Fig. 3 it can be seen that for a depletion width equal to the range of the average β ($66\mu\text{m}$) a doping concentration approximately 1×10^{11} electrons cm^{-3} is required. The analysis of this device will be based upon a depletion region width equal to the penetration depth of the average β ($66\mu\text{m}$).

B. Calculating device power

The short circuit current was calculated for this betavoltaic which is a sum of the depletion region current I_o and the substrate region current I_N . The equation used is¹⁰

$$I_{sc} = I_D + I_N = \lambda \phi \frac{E_{avg}}{E_{pair}} (\alpha_1 + \alpha_2) \quad (3)$$

Where

- λ metal penetration coefficient
- ϕ activity of the radioisotope
- q electron charge
- E_{avg} average energy of radioisotope

E_{pair} energy required to create electron hole pairs
 α_1 α_2 current contribution factors from depletion and epilayer regions

$$\alpha_1 = 1 - \exp\left(-\frac{w_d}{L_a}\right)$$

$$\alpha_2 = \frac{L_p L_a}{L_a^2 - L_p^2} \left[\left(\coth \frac{L-w_d}{L_p} - \frac{L_p}{L_a} \right) \exp\left(-\frac{w_d}{L_a}\right) - \frac{\exp(-L/L_a)}{\sinh((L-w_d)/L_p)} \right]$$

- L_a stopping range of β particles
- L_p diffusion length of minority carriers
- L n-type epilayer thickness

The open circuit voltage was then calculated using the formula¹⁰

$$V_{oc} = \frac{nkT}{q} \ln\left(\frac{I_{sc}}{I_o} + 1\right) \quad (4)$$

- n ideal factor
- I_o reverse saturation current

Calculating the open circuit voltage requires the reverse saturation current to be known. To determine the reverse saturation current the following equation was used¹⁰

$$I_o = SA^* T^2 \exp\left(-\frac{q\phi_b}{kT}\right) \quad (5)$$

Where

- S cross section area of device
- A^* effective Richardson constant
- ϕ_b Schottky barrier height

The current for these devices in operation is given by¹⁰

$$I = I_{sc} - I_o \left(\exp\left(\frac{qV}{nkT}\right) - 1 \right) \quad (6)$$

To determine performance factors of the battery such as power, fill factor and efficiency, the max power is required. This was calculated numerically using matlab given

$$\frac{\partial(IV)}{\partial V} = 0 \quad (7)$$

The max power was found and as a metric of evaluation the filling factor and efficiency of the device were calculated by the following equations

The filling factor (FF) is

$$FF = \frac{V_m I_m}{V_{oc} I_{sc}} \quad (8)$$

$$\eta = \frac{V_m I_m}{q\phi E_{\beta}} \quad (9)$$

TABLE I. Calculation Parameters

Parameter	Value	Reference
ϵ_s	9	11
N_D	$1 \times 10^{11} \text{ cm}^{-3}$	-
N_C	$2.23 \times 10^{18} \text{ cm}^{-3}$	11
ϕ_b	0.95 eV	11
k	$1.38064852 \times 10^{-23} \frac{\text{J}}{\text{K}}$	-
T	300 K	-
λ	1	-
ϕ	1mCi	-
E_{avg}	0.196 MeV	7
E_{pair}	10.17 eV	12
L_a	66 μm	-
L_p	1.5 μm	13
L	100 μm	-
S	1 cm^2	-
A^*	$26.4 \text{ A/K}^2 \text{ cm}^2$	11
n	2.9	12

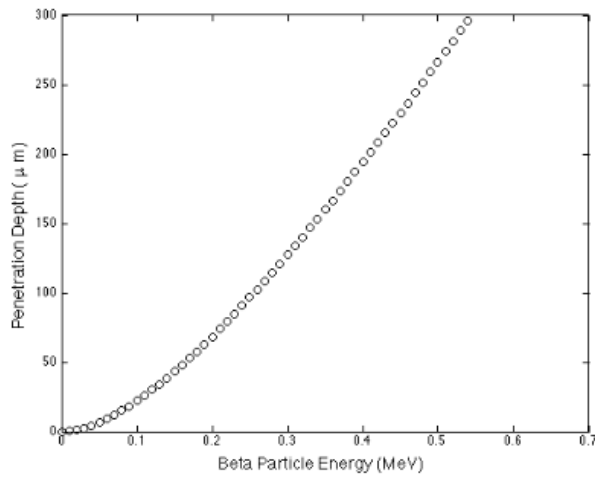


FIG. 2. Beta penetration depth in GaN as a function of energy

III. RESULTS AND DISCUSSION

Calculations using the parameters specified in Table I yielded a Schottky barrier width of 66 μm , corresponding to a N-type doping carrier concentration in the GaN of $1 \times 10^{11} \text{ cm}^{-3}$. The short circuit current I_{sc} was calculated to be 72.4 nA and the open circuit voltage was determined to be V_{oc} 0.4218V. The max power was determined to be 17.5 nW at a operating voltage of 0.31 V and current of 56.45 nA. The filling factor was determined to be 0.5732 and the efficiency of the device is 1.52% see Fig. 4. A similar GaN Schottky barrier device using Ni-63 of 1 mCi radioactivity determined a theoretical power of 4.2nW¹⁴. This shows that there is a potentially to create higher power betavoltaics using Sr-90 as the source. There are critical limitations, however in this theoretical analysis there were some factors ignored that will effect

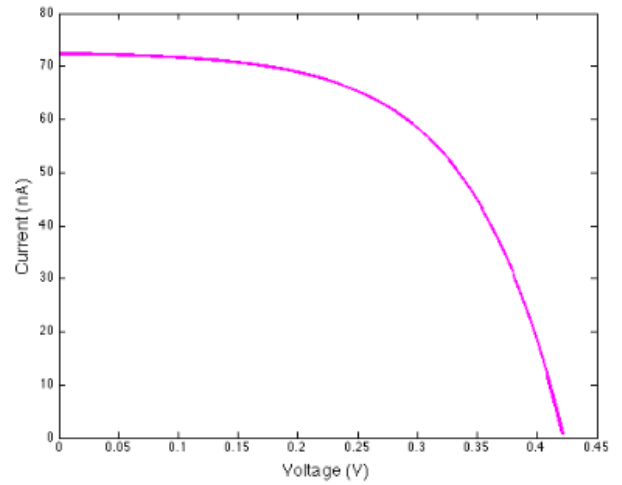


FIG. 3. Depletion region width in GaN Schottky barrier diode as a function of doping concentration N_D

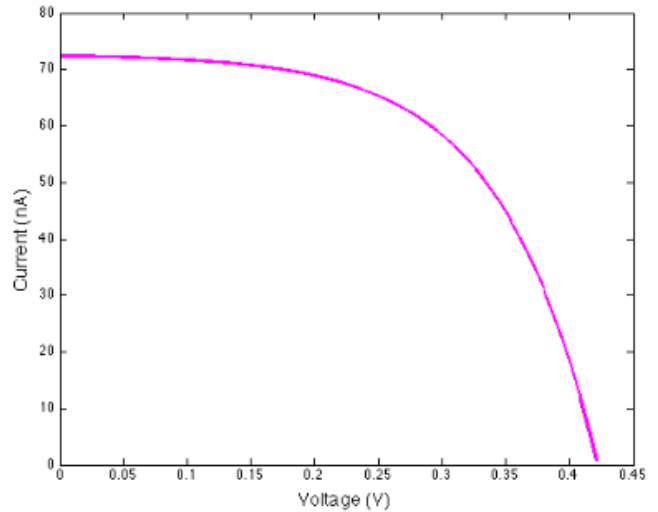


FIG. 4. I-V curve of proposed device

the operation of the device. In practice due to manufacturing limitations there is no current way of growing a GaN layer with a dopant density of $1 \times 10^{11} \text{ cm}^{-3}$. Currently the typically found values of the dopant concentration is $1 \times 10^{15} \text{ cm}^{-3}$, there are proposed methods that can potentially reduce the carrier concentration to $1 \times 10^{13} \text{ cm}^{-3}$ ¹⁴. However, at these dopant concentrations, the depletion region widths are 1 and 8.5 μm respectively. This will yield a max power of 2.48 nW . As well as a fill factor of 0.5063 and efficiency of .22%. The manufacturing limitation of GaN makes it an impractical candidate for a betavoltaic using Sr-90. Further more in this analysis it was ignored that Sr-90 decays to Y-90 another β emitter with a β_{max} of 2.28 MeV. The β penetration depth would be too large to be absorbed by the proposed nu-

clear battery.

The theoretical battery analyzed has another large limitation in practice, the radiation resistance of GaN is limited to a damage threshold of 440 KeV¹⁵. As a result, the Sr-90 would damage the GaN and will reduce the power output and efficiency of the device over time. Other semiconductors such as silicon have even lower thresholds for radiation damages (220 KeV)¹⁵ making Sr-90 an impractical source. A final consideration is the radiation emitted from the proposed battery. Due to the high energy Y-90 β , shielding is likely required, when shielding high energy β particles bremsstrahlung (braking radiation) can occur and cause highly penetrating x-rays to be emitted. Due to manufacturing limitations and radiation resistance limits of current semiconductors it is not recommended that Sr-90 be used as a radioactive isotope for nuclear microbatteries. There if materials were designed sufficiently radioactively 'hard' and were able to be made with a sufficient depletion region width, Sr-90 is a good potential isotope. It could provide more power than the commonly used Ni-63 microbattery and has a sufficiently long life with a $T_{1/2}$ of 28.8 years.

Further research to advance the nuclear battery will include the increasing the radiation resistance of semiconductor materials and for the Schottky GaN betavoltaic, an increase in power and efficiency can be achieved if manufacturing methods can reduce the dopant density in the material.

CONCLUSION

It has been demonstrated that a GaN Schottky battery using Sr-90 as a radioisotope can produce a power of 17.5 nW. This power is achieved at an operating voltage of 0.31 V and 56.45 nA, resulting in a fill factor of 0.5732 and efficiency of 1.52%. However, Sr-90 is not recommended currently as a radioisotope for beta voltaics. For Sr-90 to be a practical source for betavoltaics, semiconductors with sufficient radiation hardness and betavoltaic designs with sufficient depletion widths must be created. GaN Schottky betavoltaics provide larger amounts of radiation resistance compared to other betavoltaic designs such as P-N silicon batteries, but due manufacturing limitations cannot achieve a sufficient depletion region width. Future research to increase the performance of

betavoltaic devices should look into increasing the radiation resistance of the devices so higher energy radioisotopes such as Sr-90 can be used, as well as increasing ability to create larger depletion region widths in radiation resistant semiconductors.

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